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**Anomalous transfer phenomenon of carbon nanotube in the blend  
of polyethylene and polycarbonate**

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**1 ABSTRACT**

2 A contradict interphase transfer of multi-walled carbon nanotubes (MWCNT) is  
3 detected in the immiscible polymer pair of polyethylene (PE) and polycarbonate (PC). When  
4 laminated sheets composed of PE with MWCNTs and PC are annealed in the molten state of  
5 both polymers, MWCNTs are found to move from PE to PC. This transfer phenomenon is  
6 originated from the difference in the interfacial tension with the aid of Brownian motion. On  
7 the contrary, MWCNTs prefer to reside in the PE phase in the blend of PE, PC and  
8 MWCNTs, even when MWCNTs are first dispersed in PC. This result indicates that  
9 MWCNTs transfer from PC to PE. The opposite direction of the transfer is attributed to the  
10 PE molecules being adsorbed on the surface of MWCNTs, which are generated during  
11 mixing.

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13 **Keywords: Electrical Properties; Interphase; Thermoplastic resin; Carbon fibre;**

14 **Laminates**

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## 1 **1. Introduction**

2 Carbon nanotubes (CNTs) have been investigated in many research fields ever since  
3 their discovery by Iijima in 1991 [1]. Due to their high aspect ratio (100-1000) and specific  
4 surface area, the electrical and mechanical properties of a polymeric material can be  
5 improved by adding CNTs [2-4]. Based on the above characteristics, it is appropriate to  
6 employ CNTs as a conductive filler in polymer composites for many applications in the  
7 manufacturing such as electrostatic dissipation, interference shielding, and so on [5-7]. Of  
8 course, the electrical properties of polymer composites are affected by the dispersion of  
9 CNTs in the material, therefore it is important to understand and control the CNT dispersion  
10 [8].

11 Sumita et al. described the concept of double percolation, in which the amount of  
12 carbon blacks (CBs) is beyond the critical value for percolation in one continuous phase of an  
13 immiscible blend [9,10]. This method makes it possible to prepare a conductive composite  
14 with a small amount of CBs. Sumita et al. also revealed that CBs selectively reside in  
15 polyethylene (PE) phase in the blend of PE and poly(methyl methacrylate) (PMMA),  
16 although PE is a non-polar polymer [10]. Furthermore, Wu et al. found that the addition of  
17 PE reduces the percolation threshold of the composite with vapor-grown carbon fibers  
18 (VGCFs) in PMMA [11]. They explained that it is attributed to the self-assembled conductive  
19 network constructed by selective adsorption of PE on the end part of the VGCF filament.  
20 Later, they explained that this phenomenon is attributed to the flexibility of PE chains, which  
21 leads to the preferential adsorption at the rough ends of VGCF by entropic favor [12].  
22 Similarly, Pötschke et al. prepared a conductive blend using polycarbonate (PC) and PE with  
23 MWCNTs and found that MWCNTs act as a bridge between two polymers by the adsorption  
24 of chain ends [13]. Though, Mamunya et al. reported that the selective localization of  
25 conductive fillers in an immiscible polymer blend can be predicted by the interfacial tension

1 between polymers and conductive fillers [14]. Typically, CNTs immigrate from a polymer  
2 with high interfacial tension to another with low interfacial tension through the boundary  
3 between the phases, because CNTs show high surface tension (45 mN/m) [15]. Besides,  
4 Gubbels et al. demonstrated that the selective localization of CBs at the interphase between  
5 PE and polystyrene (PS) in the co-continuous blend can greatly reduce the content of CBs  
6 required for the percolation threshold [16]. This selective localization occurs at the specific  
7 balance of interfacial tension among polymers and fillers.

8         Recently, the imprinting technique of nanofillers from one polymer to another has  
9 been developed to modify the surface properties of polymers [17-20]. Doan et al. conducted  
10 the annealing procedure using laminated sheets composed of pure PE and polypropylene (PP)  
11 containing nanofibers of poly(butylene terephthalate) (PBT) [19]. They found that PBT fibers  
12 are transferred from molten PP to PE, which results in the surface-modified PE sheet after  
13 separation of the laminated sheets. Similarly, nanofibers of polytetrafluoroethylene (PTFE) in  
14 a molten poly(lactic acid) (PLA) are transferred from PLA to PP during the annealing  
15 procedure, although PTFE does not transfer from PP to PLA [19]. These results indicate that  
16 the localization phenomenon is attributed to the compatibility with nanofillers. Furthermore,  
17 they reported that silica nanoparticles preferentially migrate from poly(styrene-*co*-butadiene)  
18 (SBR) to poly(butadiene) (BR) phase during annealing beyond their glass transition  
19 temperatures [20]. Nevertheless, the migration from BR to SBR does not occur,  
20 demonstrating that the interfacial tension between silica and BR is lower than that between  
21 silica and SBR, i.e., the compatibility between silica and a rubber is the main driving force  
22 for the transfer.

23         In the previous paper in our research group [21], it was found that the interphase  
24 diffusion of MWCNTs from PP to PC occurs during the annealing treatment of laminated  
25 sheets composed of PP/MWCNT and PC, leading to a conductive film of PC with a

1 significantly small amount of MWCNTs. In contrast, the transfer is not detected at all from  
2 PC to PP. The results directly indicate that the interfacial tension between PC and MWCNT  
3 is lower than that between PP and MWCNT. Since the Brownian motion is required for the  
4 interphase diffusion, the annealing time and temperature are critical conditions for the  
5 transfer.

6 In this study, however, a contradict phenomenon of the MWCNT transfer from PC to  
7 PE phase was detected during melt-mixing process. Considering that MWCNTs move from  
8 PE to PC in laminated sheets composed of PE/MWCNTs and PC, these results should be  
9 noted. This study will provide the useful information on the material design using PE and  
10 carbon fillers with understanding of the driving force of PE adsorption on the fillers.  
11 Furthermore, it will be applicable to obtain high-performance polymer blends reinforced by  
12 CNTs. Since the enhancement of mechanical properties, especially rigidity, is greatly  
13 required in the field of automobiles and aircrafts, intense interest has been focused on  
14 composites with CNTs. In these applications, for example, CNTs should be localized in a  
15 matrix of rubber-modified plastics with sea-island structure.

16

## 17 **2. Experimental**

### 18 *2.1. Materials*

19 The polymers used in this study were commercially available bisphenol A  
20 polycarbonate (PC) (Panlite L-1225Y, Teijin Co., Ltd., Japan, MFR = 11 [g/10 min]) and  
21 high-density polyethylene (PE) (HJ590N, Japan Polyethylene Corp., MFR = 40 [g/10 min]).  
22 The number- and weight-average molecular weights, characterized by a size exclusion  
23 chromatograph (SEC) (Tosoh Corp., HLC-8020) using chloroform as an eluent, of PC are  $1.9$   
24  $\times 10^4$  and  $9.7 \times 10^4$ , respectively, as a polystyrene standard. Moreover,  $M_n$  and  $M_w$  of PE  
25 were also characterized by SEC using 1,2,4-trichlorobenzene at 140 °C and found to be 0.87

1  $\times 10^4$  and  $4.9 \times 10^4$ , respectively as a polyethylene standard. The density of PE is 960 [kg/m<sup>3</sup>]  
2 at room temperature.

3 MWCNTs were produced by a catalytic chemical vapor deposition method using a  
4 floating reactant method and subsequent thermal treatment up to 2,600 °C [22,23]. Typical  
5 diameters of the MWCNTs are ranging from 40 to 80 nm as shown in Fig. 1, while the  
6 lengths are between 10 and 20  $\mu$ m. The density is approximately 2,300 [kg/m<sup>3</sup>].

### 7 [Fig.1]

8 Two types of composites with 20 wt% of multi-walled carbon nanotubes (MWCNTs),  
9 i.e., PC/MWCNT and PE/MWCNT, were kindly provided by Hodogaya Chemical Co., Ltd.  
10 (Japan) as a pellet form.

11

### 12 2.2 Sample preparation

13 Pure PC and its composite with 20 wt% of MWCNTs were dried at 120 °C for 8 h in  
14 a vacuum oven before processing.

15 A composite of PC/MWCNT (80/20) was mixed with pure PE in the molten state  
16 using a 30 cc internal mixer at 250 °C for 10 min at a blade rotation speed of 50 rpm. The  
17 blend ratio of PC/MWCNT and PE was 80:20 in weight fraction, i.e., PC/MWCNT/PE =  
18 64/16/20. In addition, another blend composed of pure PC and pure PE at a blend ratio of  
19 76/24 (= 64/20) was also prepared under the same condition without MWCNTs. The obtained  
20 samples were compressed into flat sheets with a thickness of 1 mm using a laboratory  
21 compression-molding machine (Table-type test-press, Tester Sangyo Co., Ltd., Japan) at  
22 200 °C under 10 MPa for 3 min.

23 Flat sheets of PE, PC, PE/MWCNT (80/20) and PC/MWCNT (80/20) were also  
24 prepared using the compression-molding machine at 200 °C under 10 MPa for 3 min. Then,  
25 the sheets with 1 mm thickness were subsequently cooled at 25 °C. The transfer experiments

1 in the laminated sheets were conducted by placing a pure PC sheet on a PE/MWCNT (80/20)  
2 sheet (PC – PE/MWCNT). After the annealing treatment at 250 °C for 10 min, the sheets  
3 were immediately cooled and separated. The same experiment was performed using a pure  
4 PE sheet and a PC/MWCNT (80/20) sheet (PE – PC/MWCNT). This procedure was also  
5 described in detail in our previous paper [21].

6

### 7 2.3. Measurements

8 The flat sheets of PC/PE and PC/MWCNT/PE with a thickness of about 1 mm were  
9 immersed in chloroform to remove PC fraction at room temperature for three days. Then, the  
10 insoluble part in chloroform was immersed into hot-xylene to remove PE fraction at 140 °C  
11 for 6 h. The chloroform and xylene solutions with dissolved polymers were collected and  
12 subsequently dried up to characterize the dissolved parts. Furthermore, the insoluble part was  
13 dried and weighed to determine the soluble fraction  $S$ , defined by equation (1).

$$14 \quad S = \frac{w_i - w_f}{w_i} \times 100 \quad (1)$$

15 where  $w_i$  is the initial weight of the sample and  $w_f$  is the weight of the dry sample after  
16 immersion.

17 In addition, the MWCNT distribution on the surface of the insoluble part in  
18 chloroform and xylene and the surface of cryogenically fractured PC/MWCNT/PE was  
19 observed by a scanning electron microscope (SEM) (Hitachi Ltd., S4100). The surfaces of the  
20 separated PC and PE sheets at laminated experiments were also examined. Prior to the  
21 observation, all specimens were coated with Pt-Pd by a sputter coating machine.

22 The infrared (IR) spectra of pure PC and the dissolved part of the samples after  
23 extraction were measured by a Fourier-transform infrared spectroscopy (FT-IR) analyzer  
24 (Perkin Elmer Inc., Spectrum 100).



$$1 \quad \Gamma = \gamma_1 + \gamma_2 - 2\sqrt{\gamma_1\gamma_2} \quad (2)$$

2 where  $\Gamma$  is the interfacial tension between components and  $\gamma_i$  is the surface free energy of  $i$ -th  
3 component.

4 It is known that the surface free energies of PE and PC at 200 °C are 25 and 32  
5 mN/m, respectively [26]. Further, the surface free energy of MWCNTs has been reported by  
6 several researchers and was found to be larger than 45 [mN/m] [15,27,28]. The interfacial  
7 tension between the polymer and MWCNT is calculated and listed in Table 1, assuming that  
8 surface free energy of MWCNT is 45 [mN/m] [15].

### 9 [Table I]

10 It is clearly seen that the interfacial tension between PE and MWCNT is significantly  
11 higher than that between PC and MWCNT. Hence, the interphase diffusion of MWCNTs  
12 occurs only from PE to PC. The results obtained in this experiment correspond with the  
13 previous report [21].

### 14 3.2. MWCNT transfer during melt-mixing

15 The localization behavior of MWCNTs in an immiscible blend composed of PE and  
16 PC was studied using an internal mixer. In this study, MWCNTs were dispersed in PC at first  
17 (PC/MWCNT = 80/20). Then pure PE was added into the blend at 250 °C for 10 min. After  
18 compression-molding of the obtained composite (PC/MWCNT/PE = 64/16/20) at 200 °C, the  
19 sheet with 1 mm thickness was immersed into chloroform at room temperature for three days.  
20 The solution is shown in Fig. 3 with the reference samples, i.e., PC/MWCNT (80/20) and  
21 PC/PE (64/20) without MWCNTs.  
22

### 23 [Fig.3]

24 In the case of PC/MWCNT, the solution is black. This is reasonable because  
25 MWCNTs are dispersed in the solution after PC is dissolved in the solvent. For the same

1 reason, the solution of PC/PE (64/20) is opaque due to the light scattering of dispersed PE  
2 particles. In contrast, the solution of PC/MWCNT/PE (64/16/20) is fairly transparent,  
3 although PC is fully dissolved into chloroform. It should be noted because the result suggests  
4 that MWCNTs are not dispersed in the PC phase in the blend. Furthermore, it is found from  
5 the weight measurement that the insoluble part is approximately 36 wt%, which corresponds  
6 with the total amount of PE and MWCNT. Then the solution was filtrated to remove  
7 MWCNTs and/or PE by a filter paper. The filtrate solution was dried and subsequently  
8 compressed into a flat film. Thereafter, the film sample was characterized by FT-IR. It is  
9 demonstrated from the spectra in Fig. 4 that PC fraction is dissolved in chloroform.

10 **[Fig.4]**

11 Considering the weight measurement, PC fraction in PC/MWCNT/PE (64/16/20) is  
12 completely dissolved in chloroform, although MWCNTs are barely dispersed in the solution.  
13 Therefore, it can be concluded that MWCNTs are dispersed in PE phase in the blend of  
14 PC/MWCNT/PE (64/16/20). In other words, MWCNT transfer occurs from PC to PE during  
15 mixing, which is completely opposite to that detected at the laminated sheets.

16 The fractured surface of the blend, i.e., PC/MWCNT/PE, is also studied by SEM, as  
17 shown in Fig. 5. The co-continuous phase-separated structure is detected, in which only one  
18 phase, i.e., PE, contains MWCNTs.

19 **[Fig.5]**

20 To clarify the mechanism of the contradictory results, the insoluble part in chloroform  
21 is immersed into hot-xylene. Prior to the experiment, it was confirmed that pure PE is totally  
22 dissolved into hot-xylene at the same experimental condition. However, the insoluble part in  
23 chloroform, i.e., PE/MWCNT, is not completely dissolved into hot-xylene. The weight of the  
24 remaining insoluble part in hot-xylene is 23.6 wt% of the original blend (PC/MWCNT/PE).  
25 The dissolved part in hot-xylene (12.4 wt% of the original blend) is PE, which is confirmed

1 by FT-IR. Moreover, it should be noted that the solution is transparent as shown in Fig. 6,  
2 demonstrating that there are two types of PE; one is free from MWCNTs and the other is  
3 adsorbed on the MWCNT surface and forms network structure.

4 **[Fig.6]**

5 The surface morphology of the insoluble part after immersed in hot-xylene is  
6 demonstrated in Fig. 7. It is clearly seen that the shish-kebab structure, which must be PE  
7 crystals, is detected on MWCNTs. The result indicates that PE molecules adsorbed on the  
8 MWCNT surface are crystallized from MWCNTs because of the marked nucleation ability of  
9 MWCNTs as reported previously [29,30].

10 **[Fig.7]**

11 These experimental results suggest that PE molecules are adsorbed on MWCNTs  
12 during melt-mixing, presumably with the aid of oxygen. In the rubber industry, it is well  
13 known that some molecules are adsorbed on carbon blacks, which are called “bound rubber”  
14 [31-33]. Although the detail mechanism of the present system is unclear, functional groups  
15 containing oxygen on the surface of MWCNTs are responsible for the reaction and/or  
16 adsorption. In fact, PE shows branching reaction with the aid of oxygen [34]. The MWCNTs  
17 covered by PE molecules are expelled from PC phase and move to PE because of high  
18 interfacial energy between PE and PC. Therefore, mixing condition will play an important  
19 role on the distribution of MWCNTs in PC/PE blends, which greatly affects the mechanical  
20 properties in the solid state. Although the selective adsorption of PE on VGCF and MWCNT  
21 was already reported [10-13], the present results are completely different from those of  
22 previous studies. In the case of the previous studies, PE molecules are absorbed on the rough  
23 edge of fibers owing to the flexibility of PE chains. In contrast, our results demonstrate that  
24 PE molecules can be absorbed even on the flat surface of the carbon fillers as shown in Fig.  
25 1. This “in-situ surface modification” of MWCNTs will be available for the material design

1 of CNT-reinforced multi-components systems, because CNTs can be localized in a specific  
2 phase, e.g., matrix in a blend with sea-island structure.

3

#### 4 **4. Conclusion**

5 The interphase transfer of MWCNTs in the immiscible blend of PE and PC is studied  
6 by two methods; (1) annealing in the laminated sheets and (2) melt-mixing in the mixer. It is  
7 found that MWCNTs move from PE to PC during the annealing treatment in the laminated  
8 sheets. On the contrary, the interphase diffusion from PC to PE does not occur due to a large  
9 difference in the surface tension between PE and MWCNT.

10 In the case of melt-mixing, it is interesting to note that MWCNT transfer occurs from  
11 PC to PE, not from PE to PC, which has been confirmed by solvent immersion, FT-IR and  
12 SEM measurements. The contradict phenomenon is attributed to the strong adsorption of PE  
13 chains on the whole surface of MWCNTs, which will occur by the chemical reaction with the  
14 aid of oxygen during melt-mixing. The grafted PE chains on MWCNTs lead to the interphase  
15 transfer from PC to PE.

16

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23

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10

## 11 **Figure Captions**

12 **Fig. 1** SEM image of MWCNTs

13 **Fig. 2** SEM images of (a) PC surface separated from PE/MWCNT (80/20) and (b) PE surface  
14 separated from PC/MWCNT (80/20) after annealing at 250 °C for 10 min.

15 **Fig. 3** Photographs of the immersion experiment in chloroform;

16 (a) PC/MWCNT (80/20), (b) PC/PE (64/20) and (c) PC/MWCNT/PE (64/16/20)

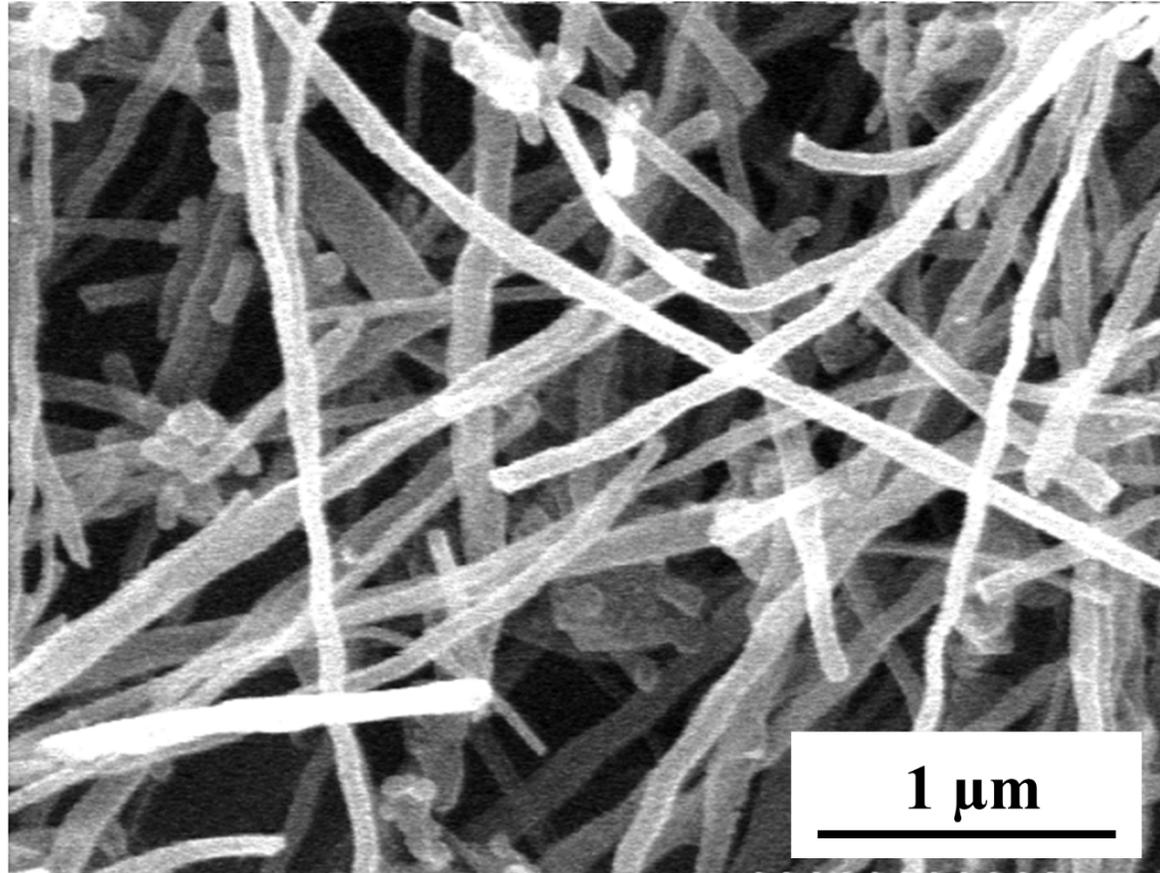
17 **Fig. 4** Infrared spectra of insoluble parts in chloroform at room temperature for (a) PC/PE  
18 (64/20) and (b) PC/MWCNT/PE (64/16/20).

19 In the figure, the spectra of pure PC and PE are also shown as references.

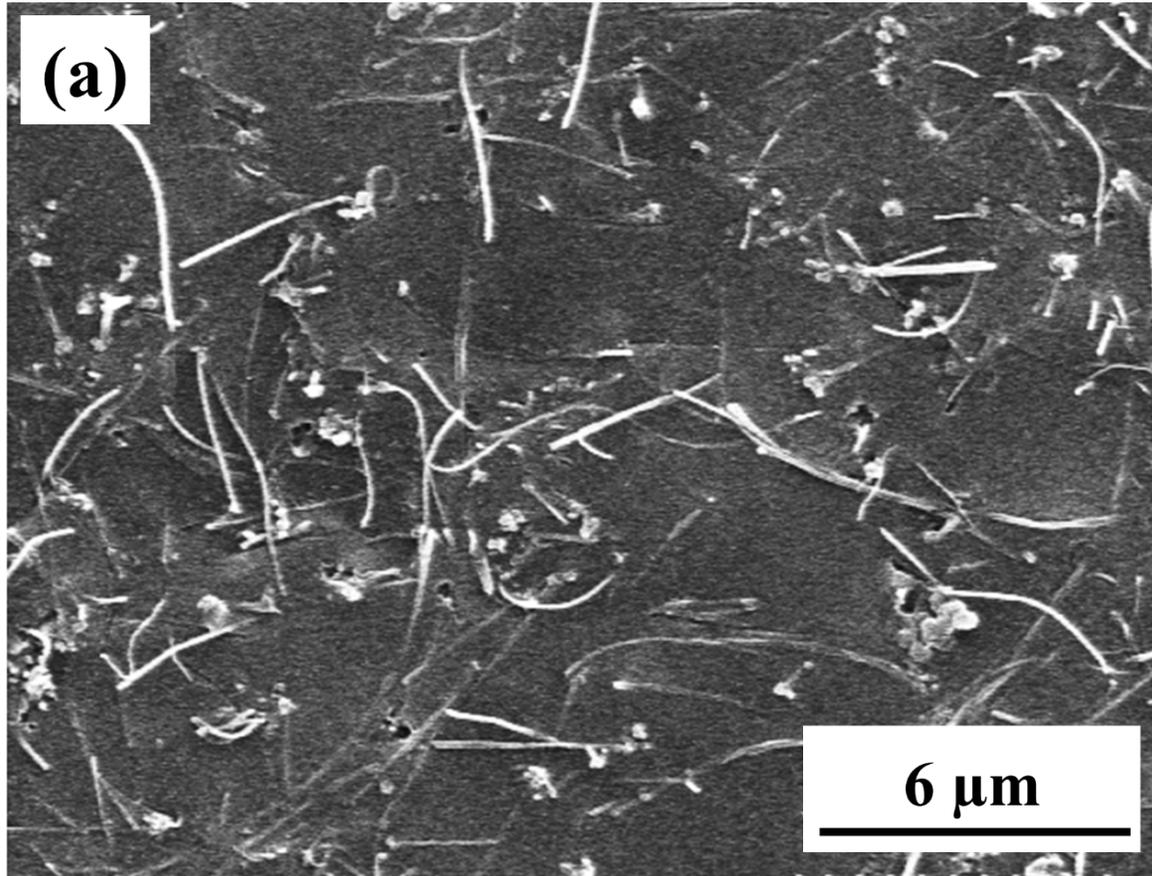
20 **Fig. 5** SEM image of fractured surface of PC/MWCNT/PE (64/16/20).

21 **Fig. 6** Photograph of the immersion experiment in hot-xylene at 140 °C for 6 hr using the  
22 insoluble part in chloroform of PC/MWCNT/PE (64/16/20).

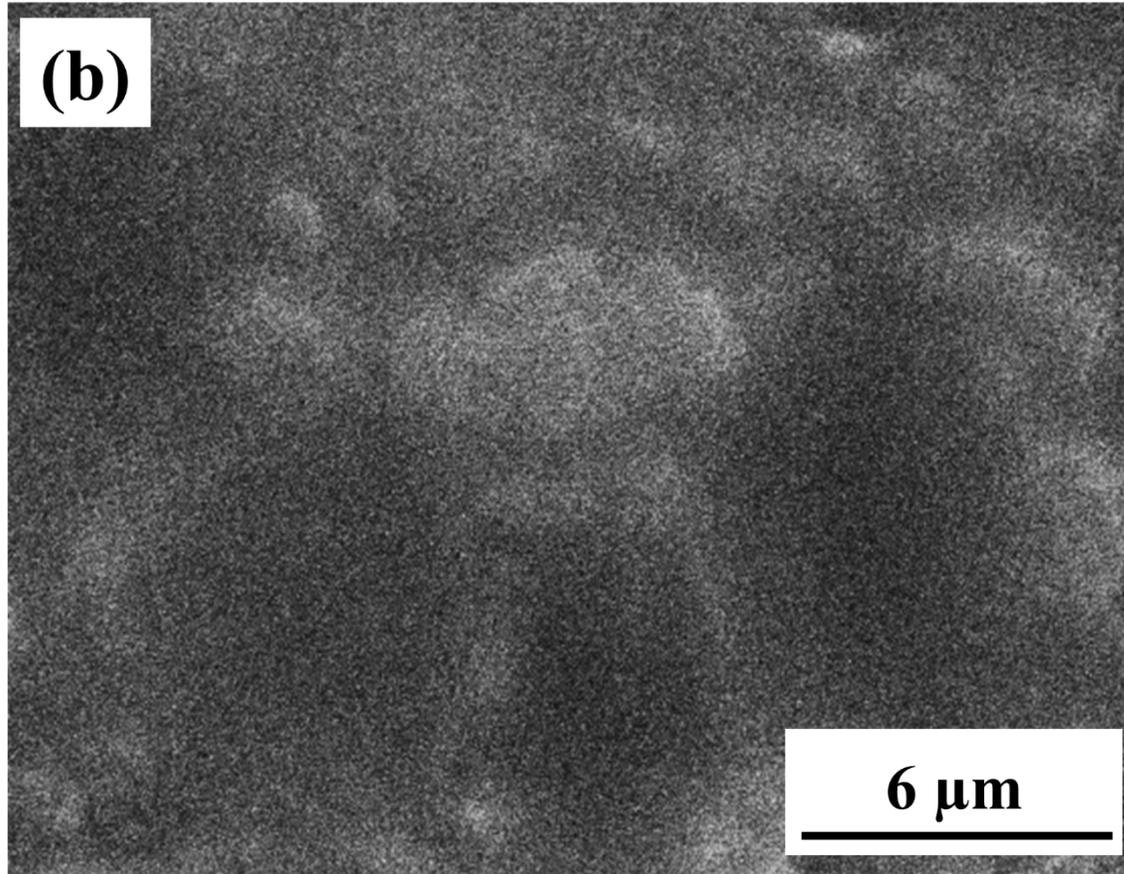
23 **Fig. 7** SEM images of the surface of PC/MWCNT/PE after extracted by chloroform and hot-  
24 xylene at different magnifications.



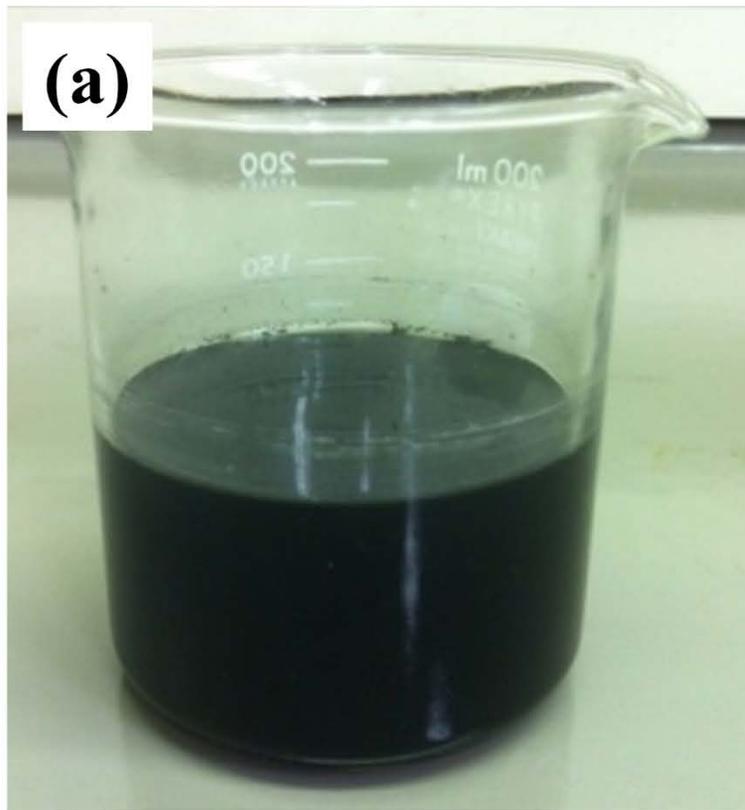
Rujirek et al., Fig. 1



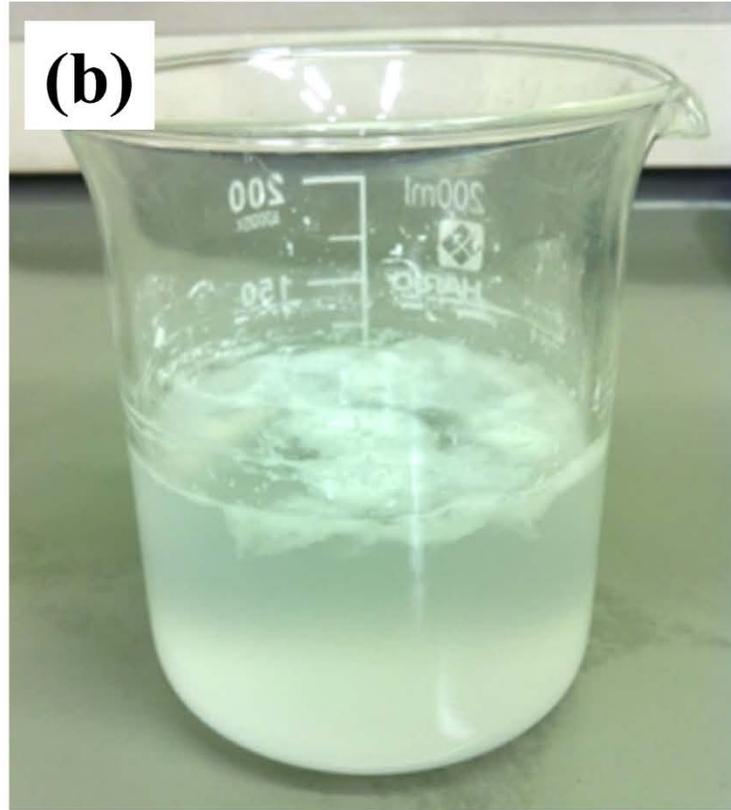
Rujirek et al., Fig. 2(a)



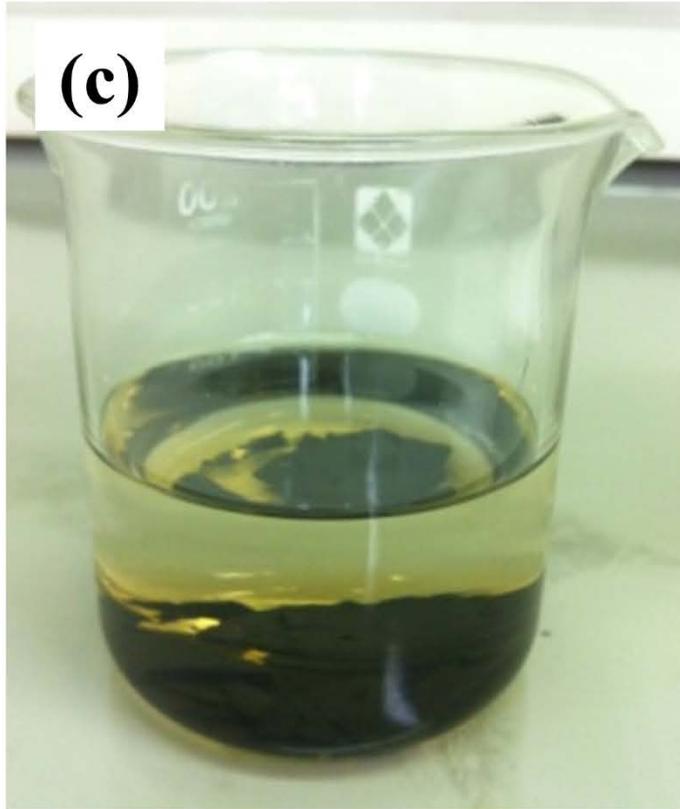
Rujirek et al., Fig. 2(b)



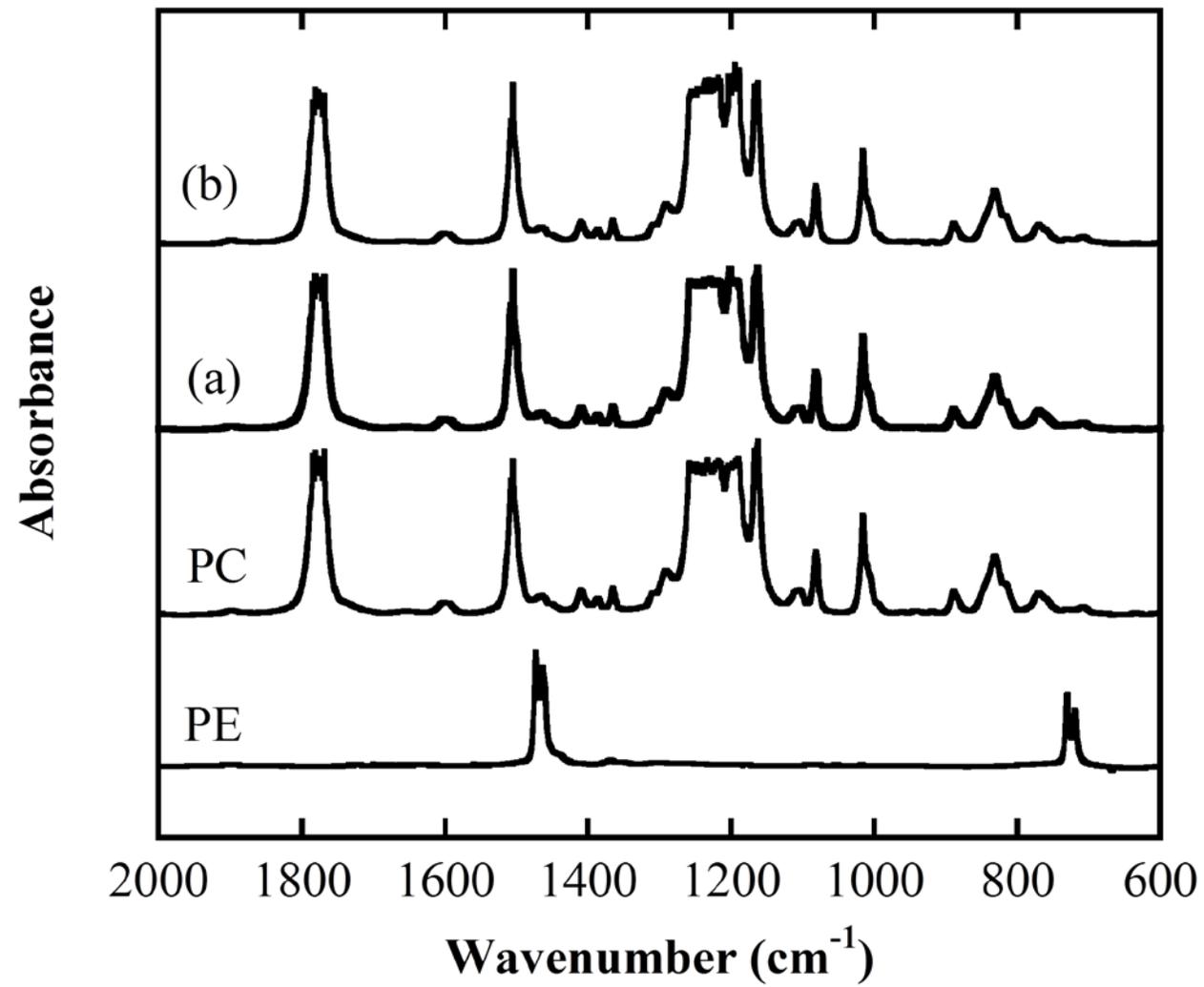
Rujirek et al., Fig. 3(a)



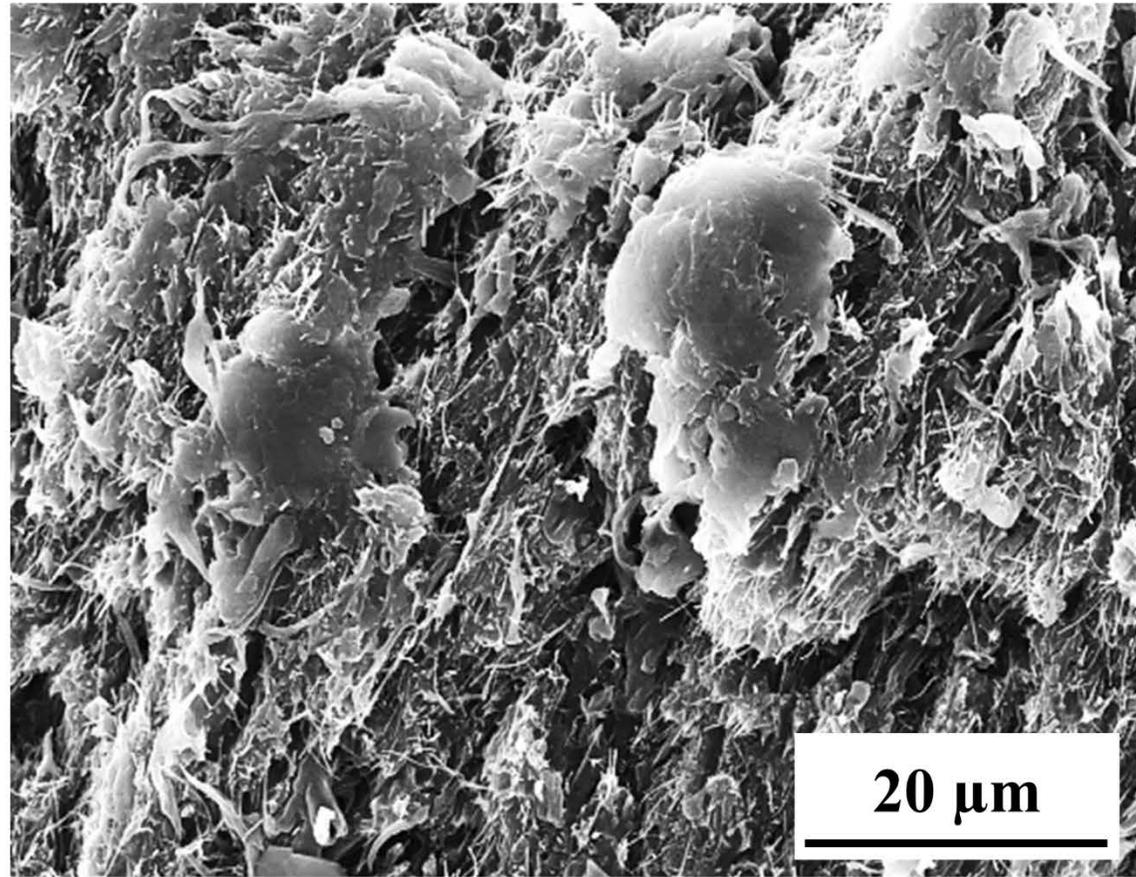
Rujirek et al., Fig. 3(b)



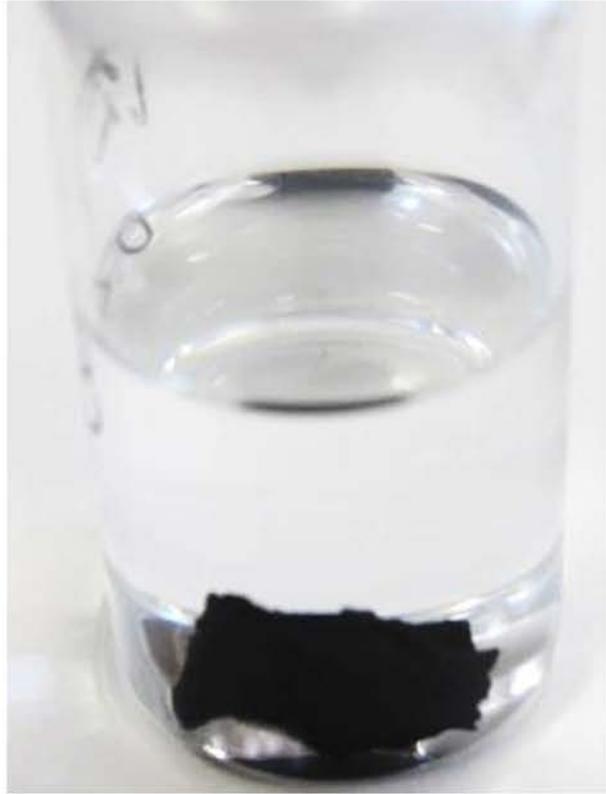
Rujirek et al., Fig. 3(c)



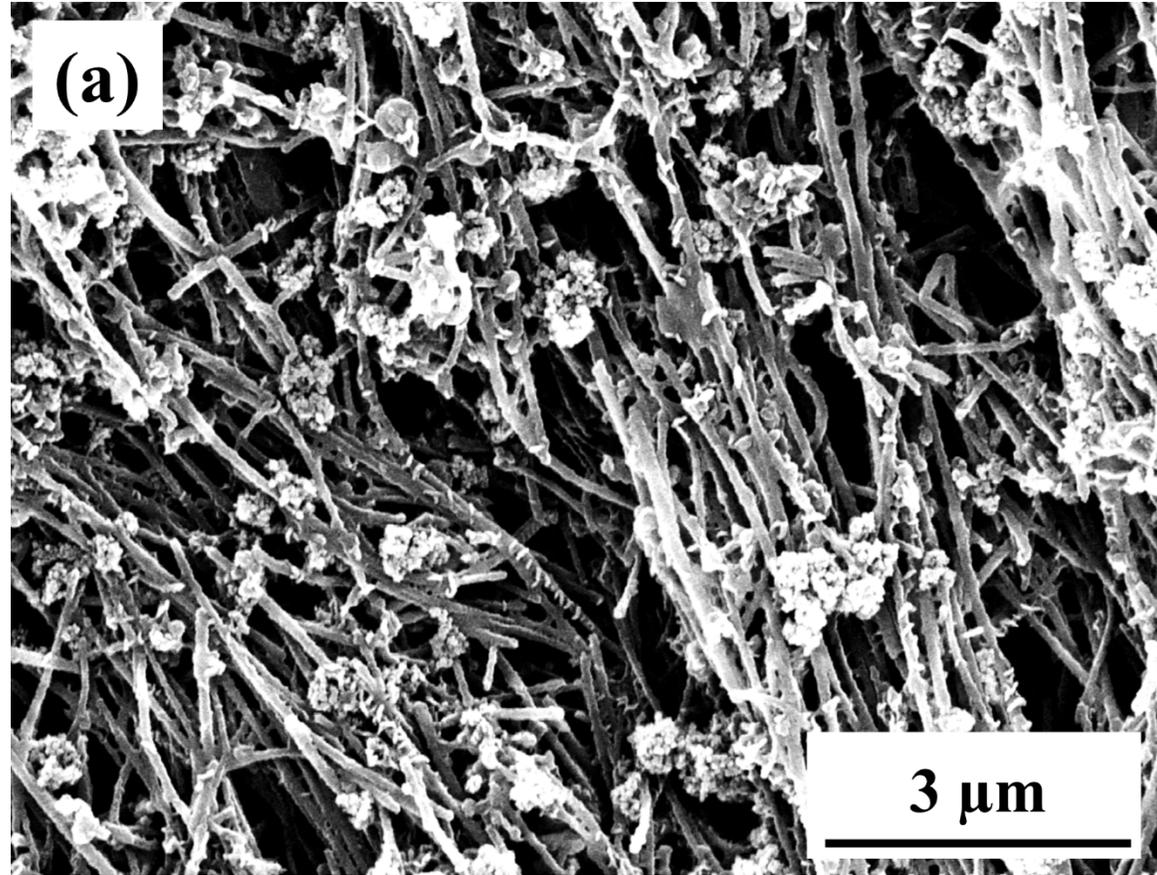
Rujirek et al., Fig. 4



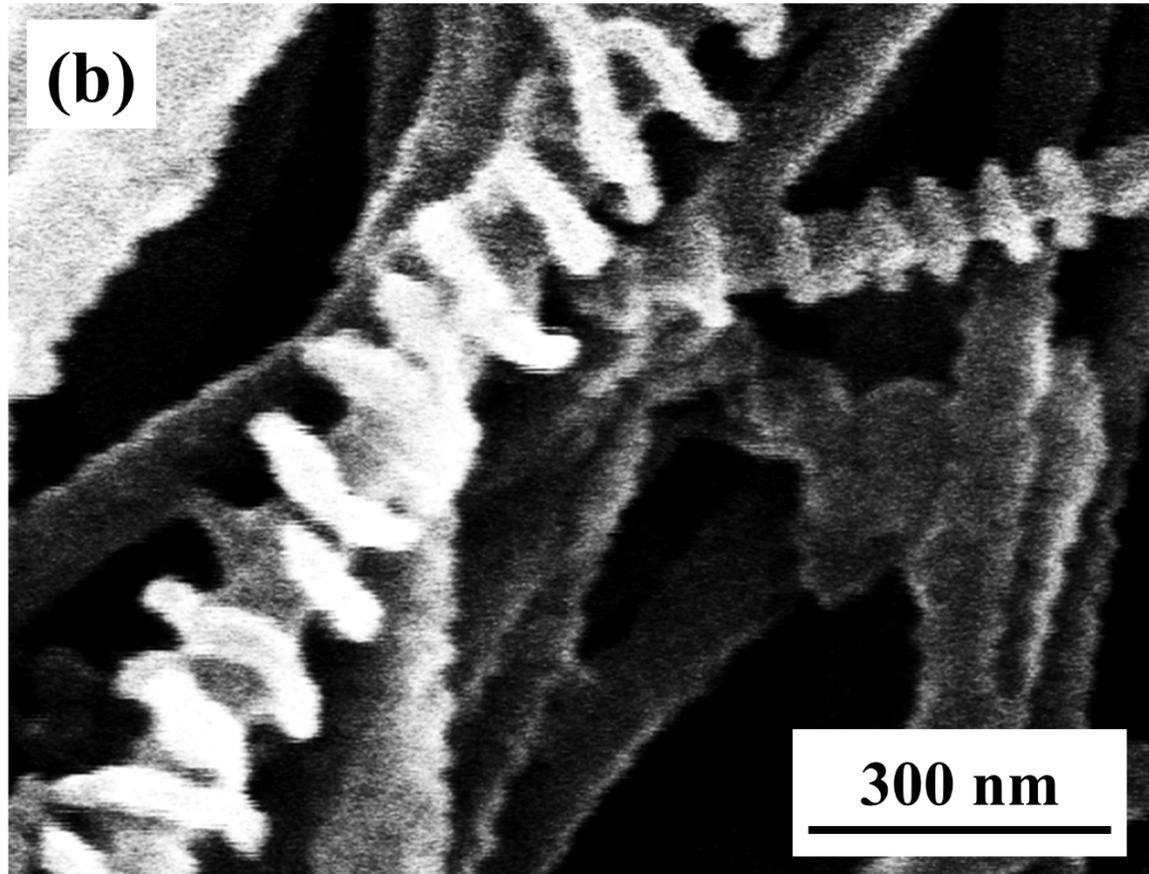
Rujirek et al., Fig. 5



Rujirek et al., Fig. 6



Rujirek et al., Fig. 7(a)



Rujirek et al., Fig. 7(b)

**Table 1** Interfacial tension  $\Gamma$  between polymers and MWCNT

$\Gamma$ (mN/m)	
PC-PE	0.431
PC-CNT	1.105
PE-CNT	2.918